

MIDDLE EAST TECHNICAL UNIVERSITY

DEPARTMENT OF ELECTRICAL AND ELECTRONICS ENGINEERING

EE463 Term Project: Wind Turbine Battery Charger

Simulation Report

Group SoC

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# ABSTRACT

To introduce the initial design of the Term Project for the EE464 Static Power Conversion II course, our group, The Isolated Ones, has compiled this simulation report. The primary objective of the term project is to create an isolated DC-DC battery charger. This report includes specified requirements, topology selection, simulation results, component selection and magnetic design.

# INTRODUCTION & SPECIFICATIONS

In this project, we are going to create isolated battery charger system from a DC source. This entails designing an DC-to-DC power converter circuit with the necessary control mechanisms. Since DC sources are not constant, we need to design a system that gives the same output voltage while the input voltage is changing. Design specifications are given below:

* Input Voltage: 20-40 V DC
* Output Voltage: 12 V
* Output Power: 60 W
* Output Voltage Peak-to-Peak Ripple: %3
* Line Regulation: %3
* Load Regulation: %3

# TOPOLOGY SELECTION

In this section, we are going to compare three topologies, which are flyback converter, forward converter, and push-pull converter to choose which topology we are going to use.

Comparison of the three converter topologies according to five different criteria is shown in Table 1. According to this table, even though the efficiency and voltage ripple of the flyback converter are worse compared to the other topologies, we chose the flyback converter topology because we won't be working with high power applications, and its lower cost and complexity are more important to us.

|  |  |  |  |  |  |
| --- | --- | --- | --- | --- | --- |
|  | **Efficiency** | **Output Ripple** | **Power Range** | **Complexity** | **Cost** |
| **Flyback Converter** | Moderate efficiency | Higher output ripple | Low to medium power | Least Complex | Cheapest |
| **Forward Converter** | Better efficiency | Lowest output ripple | Medium to high power | Medium Complexity | Medium |
| **Push-Pull Converter** | Can also have good efficiency | Moderate output ripple | Medium power | Most Complex | Most Expensive |

Table 1: Topology Comparison

# ANALYTICAL CALCULATIONS

From the previous experiences, we agreed that the most difficult part of this project to choose suitable control unit and control the switches. Due to that we fist choose a controller UC3845. We also find another controller LT3757, but it is much more expensive, so we decided to do calculations according to UC3845.

UC3845 can supply a duty cycle of 0.5 maximum, which gives us an upper boundary to choose our duty cycle. Hence, we have chosen a duty cycle range of 0.2 to 0.4. To ensure that the controller gives a duty cycle in this range, our turns ratio should be 1:1. This can be calculated as follows:

Due to the diode between the secondary side and the load, assume secondary voltage as 12.75V (= 12.75V) so that our output voltage is around 12V. Moreover, it is known that the voltage equation of a Flyback converter is as follows:

Where = 12.75 V, = 20-40 V. When = 20 and 𝑁2/ 𝑁1 ratio is taken as 1, is found as around 0.39. Furthermore, when = 40 and 𝑁2/𝑁1 ratio is taken as 1, is found as around 0.24.

For the transformer of the Flyback converter, we have selected an E-core with a gap of 1mm. The datasheet of the core can be found in the appendix section. An E-core is selected since the leakage flux in E cores is smaller than toroid cores due to their shape. Moreover, due to the existence of coil formers for each and every E-core, it is much easier to wind the coils to the core. Also, since we are to design a Flyback converter, the energy should be stored in the core first to transfer the energy to the secondary side. Hence, an E-core with a gap is required for us to implement a better solution to store the energy in the core when the switch is ON. Another reason for us to select this core is that it has a high permeability, even with the air gap, and it does not have a high volume, with a volume of 11.5 cm3, so that the core will not take up so much space in our final design. In order to find the required number of turns for both the primary and the secondary, which are the same for our design, we need to determine the magnetizing inductance value first. By using the magnetizing inductance formula in the Application Note, AN4137, Design Guidelines for Off-line Flyback Converters Using FPS [1], the magnetizing inductance can be calculated as follows:

=

where is the input power, which is selected as 72W to ensure an efficiency more that 80%, is the ripple factor, which is defined as in the Figure 1 and selected as 0.35. is the switching frequency, which was selected as 75 kHz. The core selection was done according to this frequency level. However, in order to decrease core losses, we decreased it to 75 kHz.

A diagram of a diagram of a triangle

Description automatically generated with medium confidence

Figure 1. MOSFET Drain Current and Ripple Factor

After putting the values into the equation, is found to be 20.58 µH. Then, to find the required number of turns of the primary, the value of the core is used, and the required number of turns is found by using the following formula:

Where value of the core we have selected having a 1mm of air gap is 261 nH/. Hence, after making the calculation, the required number of turns are found as 11, approximately. Moreover, by limiting the Bmax value, the minimum required number of turns can also be calculated to check whether the previously calculated number of turns is valid or not by using the formula present in [2] as follows:

where Bsat is selected as 0.2T, and effective area of the core we have selected is 125 mm2. When putting all the numbers to the equation above, it is found that minimum required number of turns should be larger than 7.77 turns (Nmin > 7.77 turns). This concludes that 11 turns in the primary and the secondary meet the requirement of minimum turns and can be used further in this design.

# MAGNETIC DESIGN RESULTS

# At first, we planned to create our own litz wire by paralleling AWG26 cables, but when we realized that we couldn't wind it as tightly as we calculated during cable winding, we chose to use ready-made litz wire. We wound the transformer with 11 turns on the primary and 11 turns on the secondary. To minimize leakage inductance, we wound the primary and secondary wires in parallel. Primary winding inductance, and leakage inductance measurements are provided in Figure 2, Figure 3 respectively.

 A white electronic device with a screen

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Figure 2.Primary Winding Inductance Figure 3.Leakage Inductance

# SIMULATION RESULTS

# To ensure the functionality of our design and choose components based on current and voltage readings, we conduct simulations using LTspice environment, incorporating non-idealities. Simulation schematic is given in Figure 4.

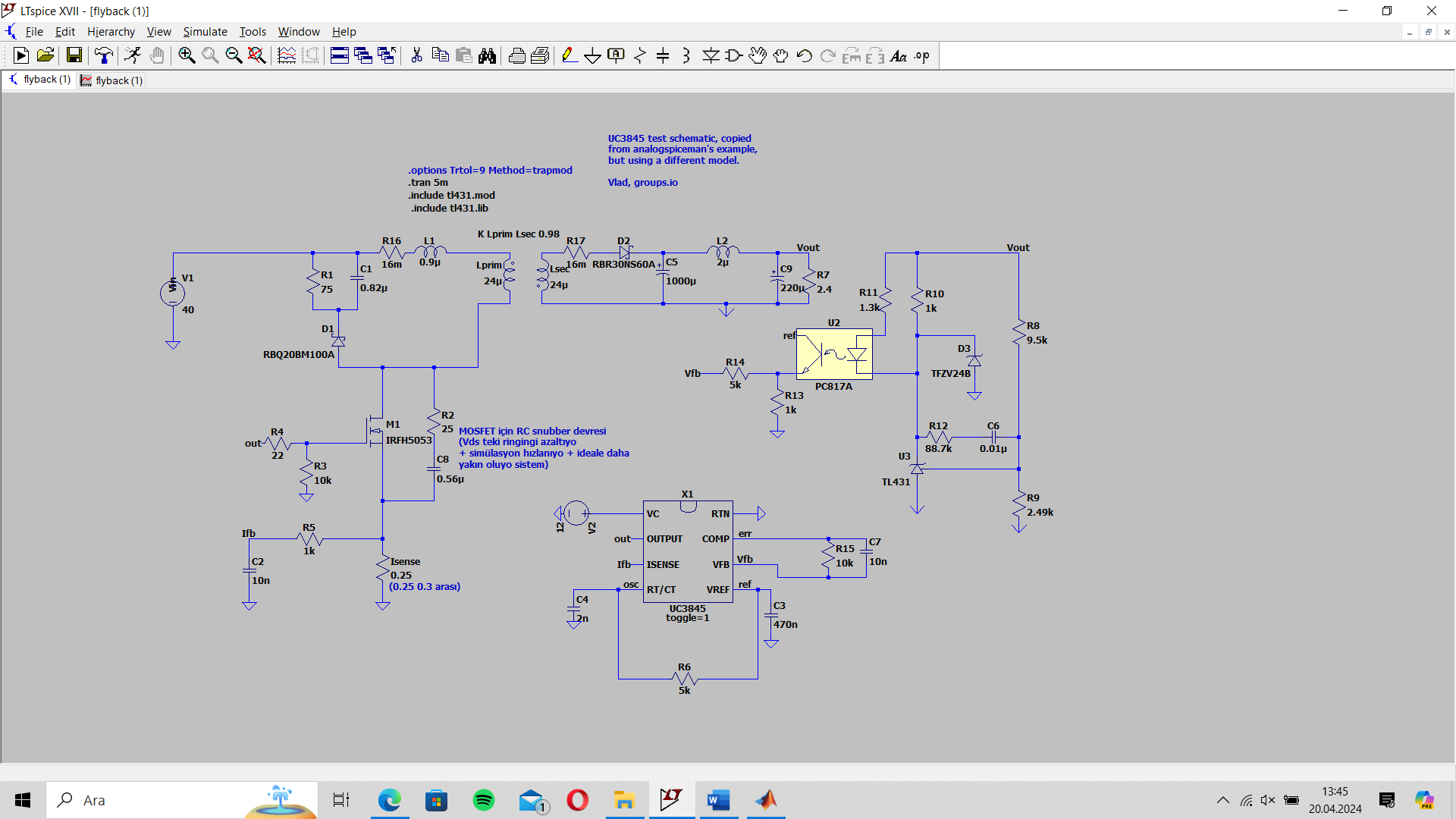


Figure 4. Simulation Schematic of Flyback Design

A screen shot of a computer

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Figure 5. Output Voltage Waveform

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Figure 6. Current passes through MOSFET (Blue) and D2 (Red)

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Figure 7.Voltage Stress on MOSFET (Blue) and D2 (Red)

Figure 5 shows the output voltage characteristic. Output inductance (L2) and capacitances (C5, C9) output voltage is much smaller than %3 of output voltage. Current passes through MOSFET (Blue) and D2 (Red) can be seen from Figure 6. As we can see from these graphs, our circuit works in CCM. Furthermore, maximum current on MOSFET is 12A and on diode is 9A. From the Figure 7, we can get maximum voltage stress on both MOSFET and the diode. The MOSFET and the diode that we will select must have voltage range greater than 70 V and 60 V respectively.

Figure 8 shows the output voltage response to changing input. In the specifications of the project, line regulation must be below to %3 which means 0.36V. When we zoom in, we can see from Figure 9 that voltage does not go below 11.64V.

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Figure 8. Output Voltage (Blue) Response to Changing Input Voltage (Green)

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Figure 9. Output Response (Blue) when the Input Voltage (Green) Change

Figure 10 shows the output voltage response to changing load current. In the specifications of the project, load regulation must be below to %3 which means 0.36V. When we zoom into steady state value, we can see from Figure 11, voltage does not go below 11.64V.

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Figure 10. Output Voltage (Green) Response to Changing Changing Load (Red) Current

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Figure 11.Output Response (Green) when the Load Current (Red) Change

# COMPONENT SELECTION

After the simulation results, we have an idea about what the voltage and current limitations of the components would be. We decided to use the following components after an extensive search.

# REFERENCES

[1]: AN-4137 Design Guidelines for Off-line Flyback Converters using FPS. Available at:

[AN-4137 Design Guidelines for Off-line Flyback Converters using FPS (dianyuan.com)](https://u.dianyuan.com/bbs/u/0/1071889497.pdf)

# APPENDIX

Link to core datasheet:

[Ferrites and accessories - ETD 39/20/13 - Core and accessories (tdk.com)](https://www.tdk-electronics.tdk.com/inf/80/db/fer/etd_39_20_13.pdf)

Link to core material datasheet:

[Ferrites and accessories - SIFERRIT material N87 (tdk.com)](https://www.tdk-electronics.tdk.com/download/528882/990c299b916e9f3eb7e44ad563b7f0b9/pdf-n87.pdf)